

**DYNAMIC NON – AXIS – SYMMETRICAL  
SUM ABOUT THE TORSION OF THE ELASTIC  
HALF-SPACE WITH THE PUNCH**

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**Summary.** In the work the sum about the joint oscillation of the elastic isotropic half-space and rigid while stretching (compression) of the punch of an arbitrary shape in the plan to which the rotational moment changing according to the harmonic law in time is applied. The asymptotic formulas for defining contact shearing stresses under the punch, the angle of lagging and module of complex amplitude of the punch oscillation.

**Keywords:** elastic half-space, integral transformations, frequency of oscillations, contact shearing stresses, complex amplitude of oscillations.

**INTRODUCTION**

Nowadays the mechanics of contact interactions of solid deformable bodies represents a big and actively developing branch of mechanics of continua. Static contact sums are quite well researched. A big problem is created by the solutions of dynamic contact sums which have a scientific and practical value.

The main publications on the given problem are given in the works [Galin 1980, Vorovich, Alexandrov, Babeshko 1974, Vorovich, Babeshko 1979, Seymov 1976, Novatskiy 1970, 1975, Kilchevskiy 1976, Cherepanov 1974, Alexandrov, Kovalenko 1986, Goryacheva, Dobychin 1988, Alexandrov, Pozharskiy 1998, Alexandrov, Chebakov 2005, Grinchenko, Meleshko 1981] which contain the review of main scientific results dedicated to the solution of contact static dynamic and thermoelastic sums for elastic and viscoelastic bodies. Mathematical methods of solution flat and spatial sums while different boundary conditions on the contact squares are set out. The main correlations of mechanics of continua and theory of elasticity are given.

**OBJECT AND PROBLEMS**

The aim of the given work is the research of dynamic non-axis-symmetrical sum about the torsion of the elastic half-space (fig. 1) with the punch and determination of

contact shearing stresses under the punch the angle of lagging and module of complex amplitude of the oscillation punch. Henceforth for shortness speaking about stresses transferences lagging their amplitude values are meant. True values are received with the multiplication by the multiplier  $e^{i\omega t}$ . As far as it is known to the authors the similar sum wasn't earlier considered.

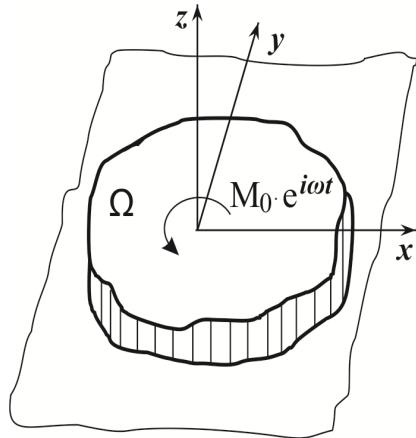


Fig. 1. The loading diagram

The use of the principle of saturable absorption [Vorovich, Babeshko 1979, Tihonov, Samarskiy 1972, Starchenko 2005, Starchenko, Buryak 2005] and twofold Fourier transform [Uflyand 1968], the given mixed sum will be led to the system of two twofold integral equations of the first type

$$\begin{aligned} \iint_{\Omega} \tau_1(\xi, \eta) K_{11}(x - \xi, y - \eta) d\xi d\eta + \iint_{\Omega} \tau_2(\xi, \eta) K_{12}(x - \xi, y - \eta) d\xi d\eta = \\ = 4\pi^2 \mu f_1(x, y), \quad (x, y) \in \Omega, \\ \iint_{\Omega} \tau_1(\xi, \eta) K_{12}(x - \xi, y - \eta) d\xi d\eta + \iint_{\Omega} \tau_2(\xi, \eta) K_{22}(x - \xi, y - \eta) d\xi d\eta = \\ = 4\pi^2 \mu f_2(x, y), \quad (x, y) \in \Omega, \end{aligned} \quad (2)$$

Here:  $\tau_1(x, y) = \tau_{xz}(x, y) = \tau_{11}(x, y) + i\tau_{12}(x, y)$ ,  $\tau_2(x, y) = \tau_{yz}(x, y) = \tau_{21}(x, y) + i\tau_{22}(x, y)$  – is shearing stresses in the area of the contact,

$$\begin{aligned} K_{11}(p, s) &= \int_{-\infty}^{\infty} \int F_1(\beta, \gamma, k) [F(\gamma, k)]^{-1} e^{i(\alpha p + \beta s)} d\alpha d\beta, \\ K_{12}(p, s) &= \int_{-\infty}^{\infty} \int F_2(\alpha, \beta, \gamma, k) [F(\gamma, k)]^{-1} e^{i(\alpha p + \beta s)} d\alpha d\beta, \\ K_{22}(p, s) &= \int_{-\infty}^{\infty} \int F_1(\alpha, \gamma, k) [F(\gamma, k)]^{-1} e^{i(\alpha p + \beta s)} d\alpha d\beta, \end{aligned}$$

### 1. Постановка задачи.

Putting the sum. From a mathematical point of view the sum comes to the solution of Lame's [Mushelishvili 1966] equation while the absence of body forces with the boundary conditions

$$\begin{cases} u = f_1(x, y, o) \\ v = f_2(x, y, o) \end{cases} \quad (x, y) \in \Omega, \quad (1)$$

$$\sigma_z(x, y, o) = 0, \quad \tau_{xz}(x, y, o) = \tau_{yz}(x, y, o) = 0, \quad (x, y) \notin \Omega.$$

Here  $u$  and  $v$  are elastic transferences on the axes  $x$  and  $y$ , and  $\sigma_z, \tau_{xz}, \tau_{yz}$  tension on the square with the normal  $z$ .

$$\begin{aligned}
F_1(\beta, \gamma, k) &= -4\beta^2\gamma^2 + (3\beta^2 + \gamma^2 - k^2)k^2 + 4\beta^2\sqrt{\gamma^2 - k^2}\sqrt{\gamma^2 - b_0^2k^2}, \\
F_2(\alpha, \beta, \gamma, k) &= \alpha\beta(4\gamma^2 - 3k^2 - 4\sqrt{\gamma^2 - k^2}\sqrt{\gamma^2 - b_0^2k^2}), \\
F(\gamma, k) &= \sqrt{\gamma^2 - k^2} \left[ 4\gamma^2\sqrt{\gamma^2 - k^2}\sqrt{\gamma^2 - b_0^2k^2} - (2\gamma^2 - k^2)^2 \right], \\
F_1(\alpha, \gamma, k) &= F_1(\beta, \gamma, k)|_{\beta=\alpha}, \quad \gamma^2 = \alpha^2 + \beta^2, \\
k^2 &= p\omega^2\mu^{-1}(1-i\varepsilon), \quad b_0^2 = (1-2\nu/2(1-\nu)).
\end{aligned}$$

$\rho, \mu$  – is the density and module of lagging of elastic half-space;

$\varepsilon$  – is the coefficient of proportionality which characterizes the internal friction;

$\nu$  – is Puassona coefficient.

For big values of the parameter  $|k|$  and bandpass area of the contact the system of equations (2) to the members of the order of values  $\frac{1}{|k|^2}$  is disintegrated into two independent equations:

$$\int_{-a}^a d\xi \int_{-\infty}^{\infty} \tau_j(\xi, \eta) d\eta \int_{-\infty}^{\infty} \frac{1}{\sqrt{\tau^2 - k^2}} e^{i[\alpha(x-\xi) + \beta(y-\eta)]} d\alpha d\beta = 4\pi^2 \mu f_j(x, y), \quad (3)$$

$$(j = 1, 2).$$

Taking into consideration that  $f_1(x, y) = -\theta y$ ,  $f_2(x, y) = \theta x$  and searching for the solution of the equations (3) accordingly in the form of

$$\tau_1(x, y) = -y\tau_1^*(x), \quad \tau_2(x, y) = \tau_2^*(x), \quad (4)$$

with the regard of the equalities

$$\frac{1}{2\pi} \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \eta e^{i\beta(y-\eta)} d\eta d\beta = y, \quad \frac{1}{2\pi} \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} e^{i\beta(y-\eta)} d\eta d\beta = 1.$$

understood in the sense of the theory of general functions [Vladimirov 1976] we will persuade that  $\tau_1^*(x)$  and  $\tau_2^*(x)$  must be found from one-dimensional integral equations of the first type which in dimensionless variables will have the look.

$$\int_{-1}^1 \tau_j(\xi) k_\varepsilon [\chi(x - \xi)] d\xi = \pi \Delta f_j^*(x), \quad (|x| \leq 1, j = 1, 2). \quad (5)$$

$$k_\varepsilon [\chi(x - \xi)] = \int_0^\infty \frac{\cos[\chi(x - \xi)] m dm}{\sqrt{m^2 - (1 - i\varepsilon)^2}}. \quad (6)$$

Here:  $\Delta = \mu a^{-1}$ ,  $2a$  – is the width of the plus punch,

$f_1^*(x) = 0$ ,  $f_2^*(x) = \theta x$ ,  $\theta = \theta_i + i\theta_2$  – is the amplitude of the angle of the turn of the punch,  $\chi = \alpha a (\rho/\mu)^{1/2}$  – is the relative frequency of the oscillations.

Using the method of work [Nobl 1962], we'll get the main member of asymptotics of solution of equations (5) for big  $\chi$ . With the regard to indications (4) while  $\varepsilon \rightarrow 0$  we'll have

$$\begin{aligned}\tau_1(x, y) &= -\Delta\theta\chi i \left[ e^{-i\chi(1+x)} / \sqrt{i\pi\chi(1+x)} + \operatorname{erf} \sqrt{i\chi(1+x)} + \right. \\ &\quad \left. + e^{-i\chi(1-x)} / \sqrt{i\pi\chi(1-x)} + \operatorname{erf} \sqrt{i\chi(1-x)} - 1 \right] y, \\ \tau_2(x, y) &= \Delta\theta\chi i \left[ \left( x - \frac{1}{2}i\chi \right) e^{-i\chi(1+x)} / \sqrt{i\pi\chi(1+x)} + \right. \\ &\quad \left. + x \operatorname{erf} \sqrt{i\chi(1+x)} + \left( 1 + \frac{1}{2}i\chi \right) e^{-i\chi(1-x)} / \sqrt{i\pi\chi(1-x)} + \right. \\ &\quad \left. + x \operatorname{erf} \sqrt{i\chi(1-x)} - x - \right], \quad \left( \operatorname{erf} x = \frac{2}{\sqrt{\pi}} \int_0^x e^{-s^2} ds \right).\end{aligned}\quad (7)$$

Further we'll define the reactive moment which acts on the punch from the side of the half-space referred to the unit of length

$$M_z' = \frac{1}{2b} \int_{-1}^1 dx \int_{-b}^b [x\tau_2(x, y) - y\tau_1(x, y)] dy = M_1' + iM_2'. \quad (8)$$

Substituting (7) and (8) we'll get

$$\begin{aligned}M_z' &= \Delta\theta \left[ (1+4xi)\operatorname{erf} \sqrt{2xi} + \sqrt{2xi}e^{-2xi} / \sqrt{\pi} - 2xi \right] / 3, \\ (M_z &= M_z' / b^2, \quad M_z = M_1' + iM_2').\end{aligned}\quad (9)$$

In the formulas (8) and (9) it's known that the punch isn't endlessly long but has the final but quite big length.

2. We'll get the formulas for counting the angle of lagging  $\varphi$  and module of complex amplitude of the oscillation of the punch  $\theta_0$ . We'll write down the equation of the rotating movement of the punch relative to the ax  $z$ .

$$J_z \cdot \frac{d^2}{dt^2} (\theta e^{i\omega t}) = M_0 e^{i\omega t} - M_z e^{i\omega t}, \quad (10)$$

where:

$$JmM_0 = 0, \quad J_z = J_z' / b^2, \quad M_0 = M_0' / b^2,$$

$J_z'$  – is the moment of the inertia of the punch relative to the ax  $z$ .

Having done the differentiation in (10) and the division of real and imaginary parts we'll get taking into consideration (9)

$$M_0 = \theta_1 (A_{11} - J_z \omega^2) + A_{12} \theta_2, \quad 0 = \theta_1 A_{21} + \theta_2 (A_{22} - J_z \omega^2). \quad (11)$$

Solving the system (11) relative to  $\theta_1$  and  $\theta_2$ , we'll find

$$\begin{aligned}\operatorname{tg}(-\varphi) &= \theta_2 / \theta_1 = A_{21}^* (\chi^2 J_z^* - A_{22}^*)^{-1}, \\ \theta_0^* &= \left[ (\chi^2 J_z^* - A_{11}^*)^2 + (A_{12}^*)^2 \right]^{-1/2}.\end{aligned}\quad (12)$$

Here:

$$\begin{aligned}
 J_z^* &= J_z(a\rho)^{-1}, \quad A_{nj}^* = A_{nj}/\Delta, \quad (n, j = 1, 2), \\
 M_1 &= (A_{11}\theta_1 + A_{12}\theta_2)\Delta, \quad M_2 = (A_{21}\theta_1 + A_{22}\theta_2)\Delta, \\
 A_{22} &= A_{11}, \quad A_{21} = -A_{12}, \quad \theta_0^* = \theta_0\Delta/M_0, \quad \theta_0 = (\theta_1^2 + \theta_2^2)^{1/2}.
 \end{aligned} \tag{13}$$

The results of the calculation of values done according to the formulas (12), (13) are given in table 1.

Table1. «The results of the calculation of the module of complex amplitude of the oscillation of the punch and the angle of lagging»

$\chi \setminus J_z^*$	$\theta_0^*$			$\varphi(pa\delta)$		
	5	10	20	5	10	20
0,125	3,785	4,476	4,623	0,890	1,165	1,891
0,250	3,635	2,421	1,028	1,555	2,413	2,855
0,375	2,074	0,907	0,403	2,378	2,835	3,007
0,500	1,043	0,463	0,215	2,722	2,960	3,058
0,625	0,612	0,282	0,134	2,862	3,014	3,081
0,750	0,403	0,190	0,092	2,933	3,044	0,094
1,000	0,214	0,104	0,051	3,002	3,074	3,109
1,250	0,133	0,065	0,032	3,034	3,089	3,116
1,500	0,091	0,045	0,022	3,053	3,098	3,120
2,000	0,051	0,025	0,012	3,075	3,109	3,125

From table 1 the dependences of values  $\varphi$  and  $\theta_0^*$  on the non-dimensional frequency  $\chi$  while different values of the non-dimensional moment of the inertia  $J_z^*$ . can be seen.

It's seen that for values  $\chi \geq 0,25$  the module of complex amplitude decreases with the increase  $\chi$  and  $J_z^*$  but the angle of lagging  $\varphi$  increases with the increase  $\chi$  and  $J_z^*$  that quiet corresponds to the physical meaning of the sum.

## CONCLUSIONS

The strict conclusion of integral equations with taking the principle of the limited absorption into consideration is received. The asymptotic formulas for defining contact shearing stresses in dependence on the amplitude of the angle of the turn of the punch which can be used for specified calculations on the durability and rigidity in transport and general machine-building are given.

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## ДИНАМИЧЕСКАЯ НЕОСЕСИМЕТРИЧНАЯ ЗАДАЧА О КРУЧЕНИИ ШТАМПОМ УПРУГОГО ПОЛУПРОСТРАНСТВА

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**Аннотация.** В работе рассматривается задача о совместном колебании упругого изотропного полупространства и жесткой на растяжение (сжатие) пластинки (штампа) произвольной формы в плане, к которой приложен крутящий момент, изменяющийся по гармоническому закону во времени. Получены асимптотические формулы для определения контактных касательных напряжений под штампом, угла сдвига фаз и модуля комплексной амплитуды колебания штампа.

**Ключевые слова:** упругое полупространство, интегральные преобразования, частота колебаний, контактные касательные напряжения, комплексная амплитуда колебаний..